

Invar[®] M93T

CONTROLLED EXPANSION ALLOY

Invar[®] M93T filler metal has been developed by ArcelorMittal Stainless & Nickel Alloys in order to perform homogeneous welding of Invar[®] M93 tubes by PAW or GTAW. The chemical composition of the welding consumable has been optimized to fulfill requirements for pipe applications at cryogenic temperatures:

Mechanical properties

- Overmatching of welded joints.
- Toughness and no embrittlement at cryogenic temperatures.

Stability and CTE

- No martensitic transformation at cryogenic temperatures.
- Low coefficient of thermal expansion between LNG temperature and 0°C.

Weldability

- No solidification and reheat cracking during multi-layer welding or cross welding.
- No defects (porosity, micro crack).
- Repair welding capacity by manual GTAW.

1. FILLER METAL

The typical chemical composition of Invar[®] M93T filler metal is shown in table 1.

| Typical values : Filler metal Invar M93T | | | | | | | |
|--|-----|-----|--------|-------|----------|----------|---------|
| Ni | Ti | Mn | Si | C | S | P | Fe |
| 43 | 2.5 | 0.1 | < 0.25 | 0.007 | < 0.0015 | < 0.0070 | Balance |

Table 1

2. WELDING PROCEDURE

The choice of welding process depends on the thickness of Invar[®] M93 base metal.

- Thickness < 5 mm: perform PAW process with filler metal.
- Thickness ≥ 5 mm: perform PAW process with filler metal + GTAW with filler metal.

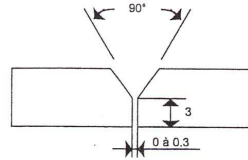
Repairs can be performed by multi-layer GTAW.

Whatever the welding process, the most important point is to employ a dilution ratio of about 30% of the filler metal Invar[®] M93T in the fusion zone:

$$\text{Dilution ratio in fusion zone} = \frac{\text{Volume of filler metal}}{(\text{Volume of filler metal} + \text{Volume of base metal})} = 25\% \text{ to } 35\%$$

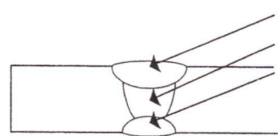
Edge preparation is recommended as indicated in figure 1 but not is necessary. Interpass cleaning by grinding and brushing is preferable to remove oxidation during the welding process.

Edge preparation



Automatic :

- PAW (1)
- GTAW (2) and (3)



Manual :

- GATW (1), (2), (3), (4)

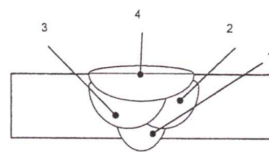


Figure 1

The range of welding specifications for Invar[®] M93T are indicated in table 2:

| Welding Procedure | | PAW Automatic | GTAW Automatic | GTAW Manual |
|----------------------------|--------------------------------|----------------------------------|---|--|
| Base metal | | Invar M93 | | |
| Filler metal | | Invar M93T (Φ = 1,2 mm) | | Invar M93T (Φ = 1,2 mm) (twist-joint) |
| Gas | Plasma (l/mn) | Ar + 2%H ₂ (3 to 5) | - | - |
| | Annular (l/mn) | Ar + 5%H ₂ (20 to 40) | - Ar + 30%He (15 to 40) - Ar + 5%H ₂ (15 to 30) | Ar (10 to 20) |
| | Backing (l/mn) | Ar (20 to 40) | - | - |
| Electrical Characteristics | Current (A) : DC (-) | 150 to 250 | 150 to 250 | 140 |
| | Voltage (V) | 25 to 30 | 10 to 20 | 14 to 16 |
| | Heat input (kJ/cm) | 9 to 23 | 4 to 15 | 10 to 20 |
| Technique | Initial and interpass cleaning | grinding - brushing | | |
| | Travel speed (cm/mn) | 20 to 25 | 20 to 25 | 7 to 10 |
| | Filler metal speed (cm/mn) | 100 to 300 | 50 to 150 | 10 to 15 |

Table 2

3. MACROSTRUCTURES AND CHEMICAL COMPOSITION

The mechanical properties, stability, CTE, and weldability are the results of the specific chemical composition of welded joints (see table 3). More precisely:

- **overmatching** and **low CTE** are the result of a compromise in titanium content. Addition of titanium improves mechanical properties of the fusion zone, by strain hardening, but impairs CTE. Figure 2a and 2b show that the micro-hardness is higher in the fusion zone than in the base metal. Optimum titanium content of the welded joint is roughly 1%.

- **Stability** with respect to martensitic transformation is improved by the high mean nickel content of the fusion zone (37% to 41%).
- **Weldability** is closely related to the low sulfur content of both filler metal and base metal.

| Typical values : Welded joint | | | | | | | |
|-------------------------------|--------------|-------|--------|--------|----------|----------|---------|
| Ni | Ti | Mn | Si | C | S | P | Fe |
| 37 to 41 | 0.75 to 1.25 | < 0.4 | < 0.25 | < 0.04 | < 0.0015 | < 0.0070 | Balance |

Table 3: Chemical composition of welded joints obtained by automatic PAW + GTAW or manual GTAW.

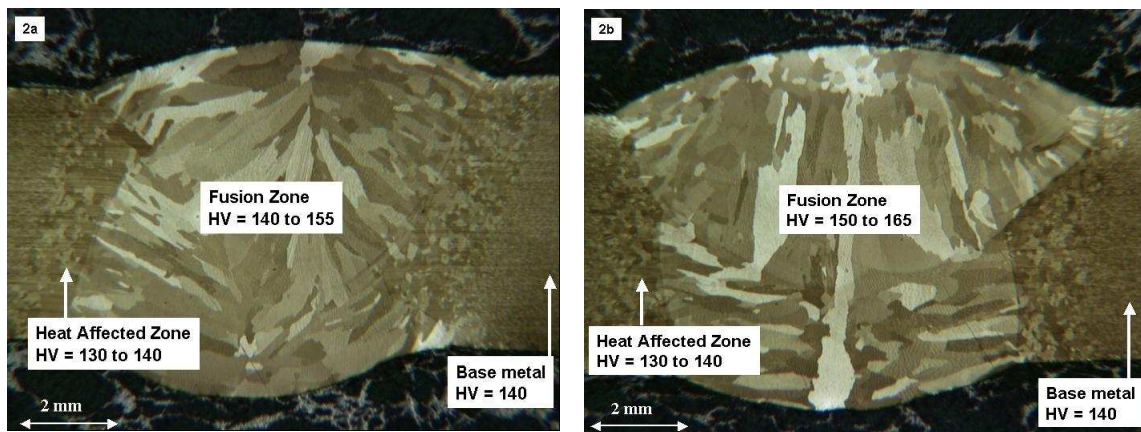


Figure 2: Cross section of welded joints performed in industrial condition. (a) automatic PAW + GTAW. (b) Manual GTAW. The micro-hardness of the fusion zone is higher than that of the base metal.

4. MECHANICAL PROPERTIES

The filler metal Invar[®] M93T gives rise to excellent mechanical properties either in case of automatic welding or manual (repair welding). Table 4 indicates high UTS and toughness at cryogenic temperatures.

| Base metal = Invar M93 Filler metal = M93T | | 0.2%YS (MPa) | UTS (MPa) | KCV (J/cm ²) | Face-Bend Root-Bend |
|---|--------|-----------------|--------------|-----------------------------|------------------------|
| Automatic PAW + GTAW | 25°C | 270 | 475 | 235 | No defect |
| | -196°C | 620 | 815 | 160 | - |
| Manual GTAW | 25°C | 290 | 486 | 210 | No defect |
| | -196°C | 670 | 805 | 150 | - |

Table 4

5. COEFFICIENT OF THERMAL EXPANSION

Expansion tests performed at low temperatures give information on stability with respect to martensitic transformation. As shown on figure 3, the welded joint obtained with Invar[®] M93T filler metal is quite stable down to -196°C .

Moreover, the CTE between -163°C to 0°C of welded joints is less than $2.9 \cdot 10^{-6}/^{\circ}\text{C}$ meanwhile the CTE of Invar[®] M93 base metal is $1.4 \cdot 10^{-6}/^{\circ}\text{C}$. So, the difference in CTE is of about $1.5 \cdot 10^{-6}/^{\circ}\text{C}$.

As a conclusion, assuming an elastic modulus of the welded joint in the range of 155 000 MPa, the maximum thermal stress can be estimated to: $\sigma = E \times \Delta\alpha \times \Delta T \sim 38 \text{ Mpa} \ll 0.2\% \text{YS}$

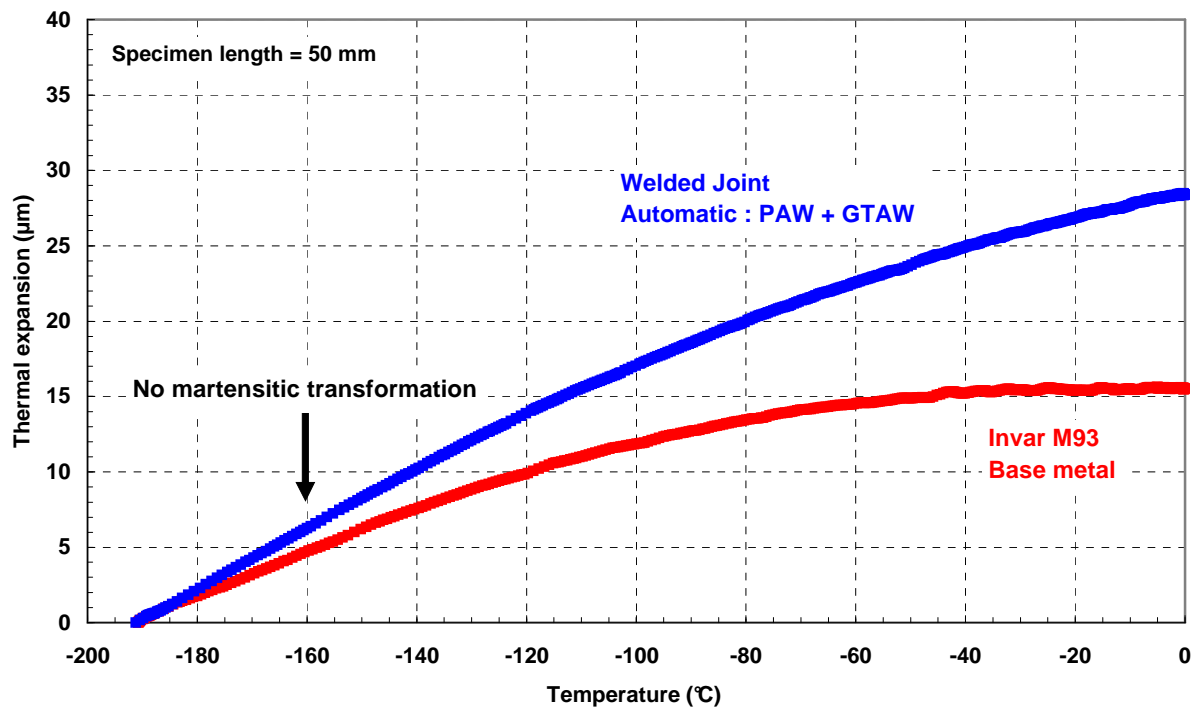


Figure 3